

Polymer Communication

# Differential scanning calorimetry of isotactic polypropene at high CO<sub>2</sub> pressures

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## Abstract

Compressed CO<sub>2</sub> gas (1–94 bar) depresses both the crystallisation temperature ( $T_c$ ) and the melting temperature ( $T_m$ ) of isotactic polypropene (iPP). The  $T_c$  of CO<sub>2</sub>-treated iPP decreases linearly with a  $dT_c/dP$  value of  $-0.18$  K/bar. Similar to  $T_c$ , the  $T_m$  of CO<sub>2</sub>-treated iPP decreases linearly with a  $dT_m/dP$  value of  $-0.12$  K/bar. Experimental  $\Delta T_m (= T_m - T'_m)$  values, where  $T'_m$  is the melting temperature at a CO<sub>2</sub> pressure of 1 bar, coincide with those predicted on the basis of the Flory–Huggins theory. © 2000 Published by Elsevier Science Ltd. All rights reserved.

**Keywords:** Isotactic polypropene; Differential scanning calorimetry; CO<sub>2</sub> pressure

## 1. Introduction

Considerable attention has been paid recently to the thermodynamic behaviour of polymers in contact with high pressure gases or supercritical fluids as an important factor in several new process applications (for example see Ref. [1]). It is important to study the pressure dependence of the glass-transition temperature,  $T_g$ , the melting temperature,  $T_m$ , and the crystallisation temperature,  $T_c$ , since these thermodynamic parameters are the main factors limiting temperatures in practical use. In fact, CO<sub>2</sub> has been shown to be a very effective plasticiser that can lower  $T_g$  [2–4] and, in some cases, can induce crystallisation of semicrystalline polymers at lower temperatures [5–7]. To the best of our knowledge, however, in situ studies on the CO<sub>2</sub>-induced shift of  $T_m$  and  $T_c$  of semicrystalline polymers using a high pressure calorimeter have been limited to poly(phenylene sulfide) [8], poly(ethylene terephthalate) (PET) [9,10] and syndiotactic polystyrene (sPS) [9]. Here we investigated the effect of CO<sub>2</sub> pressure on the melting and crystallisation behaviours of isotactic polypropene (iPP) for the following reasons: (1) for iPP a variety of physicochemical data are readily available such as the solubility of CO<sub>2</sub> in bulk iPP at high pressures, the equilibrium melting temperature, and the

equilibrium heat of fusion; (2) by utilising these data we can compare our experimental results with the thermodynamic model proposed by Flory [11,12].

## 2. Experimental

### 2.1. Materials

iPP ( $M_w = 1.33 \times 10^5$ ,  $M_w/M_n = 3.2$ ,  $[mmmm] = 0.86$ ) was purchased from Aldrich. CO<sub>2</sub> gas (>99.99% purity) was obtained from Ekika Tansan Co. Ltd.

### 2.2. Procedure

Differential scanning calorimetry of iPP was carried out on a Tian–Calvet type SETARAM C80II calorimeter [13]. The calorimeter was calibrated by carrying out the measurement of the heat of fusion of tin (literature value:  $+7.03$  kJ/mol [14]) under ambient and high pressures. About 170 mg of a polymer sample was heated to 250°C at a rate of 2 K/min, and was annealed at this temperature for 1 h. After the annealing, the system was cooled to 100°C at a rate of 1 K/min and kept at the same temperature for 1 h. The sample then was heated to 250°C again at 2 K/min.  $T_m$  and  $T_c$  were taken in the second heating process and the first cooling process, respectively. X-ray diffraction analysis (XRD) was performed on a Rigaku RINT-1200 X-ray diffractometer.

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Table 1  
Effect of compressed CO<sub>2</sub> on the melting and crystallisation behaviours of isotactic polypropene

Pressure (bar)	Heating			Cooling		
	$T_m$ (°C)	$T_m(\text{onset})$ (°C)	$\Delta H_m$ (J/g)	$T_c$ (°C)	$T_c(\text{onset})$ (°C)	$\Delta H_c$ (J/g)
1	180	166	92	131	136	-97
10	179	163	89	130	135	-97
20	177	160	92	127	133	-97
36	175	155	90	125	131	-95
50	175	152	84	122	128	-91
78	171	149	81	117	124	-90
88	169	148	76	116	123	-86
94	169	145	88	115	122	-84

### 3. Results and discussion

Table 1 summarises the pressure dependence of  $T_m$ , the melting onset temperature,  $T_m(\text{onset})$ ,  $T_c$ , and the crystallisation onset temperature,  $T_c(\text{onset})$ , as well as the heat of fusion and crystallisation for iPP. In our study,  $T_m$  and  $T_c$  are expressed as the minimum-endo- and maximum-exothermic temperatures reached during melting and crystallisation, respectively. Both  $T_c$  and  $T_m$  barely shifted in the subsequent heating-cooling cycles (up to four times). The shape of the exothermic peak due to crystallisation was independent of CO<sub>2</sub> pressure, but  $T_c$  decreased almost linearly with an increase in CO<sub>2</sub> pressure with a slope of -0.18 K/bar. The heat of crystallisation ( $\Delta H_c$ ) as well as the heat of melting ( $\Delta H_m$ ) showed a tendency to become smaller with increasing pressure, indicating a decrease in crystallinity of the CO<sub>2</sub>-treated iPP. XRD analysis showed that treatment of the iPP sample with CO<sub>2</sub> (up to 94 bar) caused no significant change in the basic morphology of the crystalline phase ( $\alpha$  form).

Table 1 also shows that the exposure to CO<sub>2</sub> brought about a shift of both  $T_m(\text{onset})$  and  $T_m$ . The shift of  $T_m(\text{onset})$  was larger than that of  $T_m$ , and therefore the melting endothermic peak broadened slightly as the CO<sub>2</sub> pressure

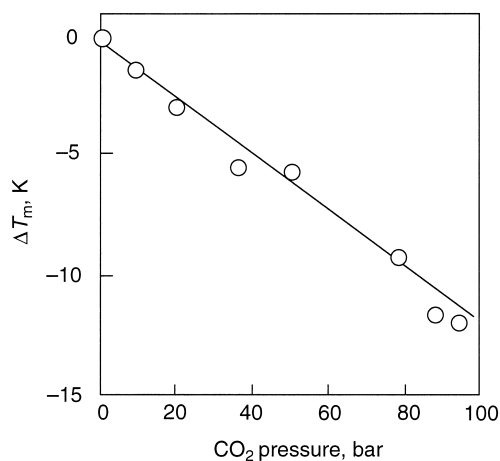


Fig. 1. Dependence of  $\Delta T_m$  of isotactic polypropene on CO<sub>2</sub> pressure. The solid line indicates the values predicted from Eq. (5).

increased. In Fig. 1, values for  $\Delta T_m = T_m - T'_m$ , where  $T'_m$  is the melting temperature at the CO<sub>2</sub> pressure of 1 bar, were plotted against the CO<sub>2</sub> pressure. It is worth noting that  $\Delta T_m$  decreased linearly with an increase in the pressure of CO<sub>2</sub> gas. The linear dependence of  $\Delta T_m$  on the pressure of CO<sub>2</sub> gas is in contrast to those of PET [9] and sPS [9].

According to the Flory-Huggins theory,  $T_m$ s of plasticised semicrystalline polymers with sufficiently high molecular weights can be correlated to the volume fraction of the plasticiser ( $v_1$ ), as shown in Eq. (1) [11,12]:

$$\left(\frac{1}{T_m} - \frac{1}{T_m^0}\right)\left(\frac{1}{v_1}\right) = \frac{R}{\Delta H_m^0} \left(\frac{V_{2u}}{V_1}\right)(1 - \chi v_1) \quad (1)$$

where  $T_m^0$ ,  $V_1$ ,  $V_{2u}$ ,  $\chi$ ,  $\Delta H_m^0$ ,  $R$  are the equilibrium melting temperature of the polymer of interest, the molar volume of CO<sub>2</sub>, the molar volume of the repeating unit of the polymer, the interaction parameter, the equilibrium heat of fusion, and the gas constant, respectively. From Eq. (1),  $T_m$  can be written as follows:

$$T_m = \frac{T_m^0}{1 + K(v_1 - \chi v_1^2)} \quad (2)$$

where  $K = (RT_m^0/\Delta H_m^0)(V_{2u}/V_1)$ . When  $v_1$  values are much less than unity, the  $v_1^2$  term is negligible. Thus,  $T_m$  is expressed by Eq. (3):

$$T_m \approx \frac{T_m^0}{1 + K v_1} \approx T_m^0(1 - K v_1) \quad (3)$$

We can calculate the volume fraction of CO<sub>2</sub> in the iPP sample from the solubility data. Fardi et al. have reported that the solubility of CO<sub>2</sub> in iPP obeys Henry's law over a CO<sub>2</sub> pressure range of 5–20 MPa, and Henry's constant ( $H$ ) of the iPP/CO<sub>2</sub> system is found to be independent of temperature [15]. Thus, the  $v_1$  at  $P$  (bar) is:

$$v_1 = \frac{wHP \frac{V_r}{V_{ig}}}{wHP \frac{V_r}{V_{ig}} + \left(\frac{w}{\rho}\right)} \approx \frac{wHP \frac{V_r}{V_{ig}}}{\left(\frac{w}{\rho}\right)} = \frac{V_r}{V_{ig}} \rho HP \quad (4)$$

where  $w$ ,  $\rho$ ,  $V_{ig}$  and  $V_r$  are the weight, the specific gravity of the polymer sample employed, the molar volume of the

ideal gas ( $= 22,400 \text{ cm}^3$ ) and the molar volume of the  $\text{CO}_2$  dissolved in the polymer, respectively.

The iPP sample employed here had a number-average degree of polymerisation of ca. 2500, and under our condition  $v_1$  values were found to be at most 0.07. Therefore, the Flory–Huggins equation (Eq. (1)) and Eq. (3), which is derived from Eq. (1), can be applied to this system. By substituting Eq. (4) for Eq. (3),  $\Delta T_m$  can be written as follows:

$$\Delta T_m = T_m - T'_m = -T_m^0 \frac{V_r}{V_{ig}} \left( \frac{RT_m^0}{\Delta H_m^0} \right) \left( \frac{V_{2u}}{V_1} \right) \rho H P + (T_m^0 - T'_m) \quad (5)$$

Thus, it should be noted that  $\Delta T_m$ , or  $T_m$ , of this system is expected to decrease linearly with the increase in  $\text{CO}_2$ -pressure.

The solid line in Fig. 1 indicates the  $\Delta T_m$  values predicted from Eq. (5) by using a  $V_1$  value of  $45 \text{ cm}^3$  [16], an  $H$  value of  $0.4 \text{ cc(STP) g}^{-1} \text{ bar}^{-1}$  [15], a  $T_m^0$  of  $460.65 \text{ K}$  [17] and  $\Delta H_m^0$  of  $165.3 \text{ J/g}$  [18]. The  $V_{2u}$  value can be estimated from the literature [17], and in this discussion, the  $V_r$  value of  $45 \text{ cm}^3$  was used [19]. In the Flory–Huggins equation thermodynamic equilibrium  $T_m$ s are used, and the thermodynamic equilibrium  $T_m$ s are generally higher by several degrees than  $T_m$ s obtained at normal scanning rates ( $1\text{--}20 \text{ K/min}$ ). Though our experimental  $T_m$ s are not thermodynamic equilibrium  $T_m$ s, we focused on the difference between two  $T_m$ s, both of which were measured under identical conditions, and the comparison of our experimental  $\Delta T_m$  values with Eq. (5) is valid. As can be seen in Fig. 1, Eq. (5) agrees very well with the experimental  $\Delta T_m$  values over the whole  $\text{CO}_2$  pressure range examined. The slope of the  $\Delta T_m$ -pressure plot was  $-0.12 \text{ K/bar}$ . This result shows that Eq. (5) is applicable to the prediction of the  $T_m$  values of the iPP/ $\text{CO}_2$  system and the interaction between iPP and  $\text{CO}_2$  is weak.

Handa et al. attributed the levelling behaviour of  $T_m$  of the sPS/ $\text{CO}_2$  and the PET/ $\text{CO}_2$  systems to the antiplasticisation effect of the hydrostatic pressure of  $\text{CO}_2$  [2,9]. In contrast, in our iPP/ $\text{CO}_2$  system this was not the case and linear dependence of  $T_m$  on  $\text{CO}_2$  pressure was shown. Consequently, the antiplasticisation effect of compressed  $\text{CO}_2$  is expected to be much smaller in the iPP/ $\text{CO}_2$  system than in the sPS/ $\text{CO}_2$  and the PET/ $\text{CO}_2$  systems.

In summary, compressed  $\text{CO}_2$  gas ( $1\text{--}94 \text{ bar}$ ) depresses both the crystallisation temperature ( $T_c$ ) and the melting temperature ( $T_m$ ) of iPP. The  $T_c$  of  $\text{CO}_2$ -treated iPP decreases linearly with a  $dT_c/dP$  value of  $-0.18 \text{ K/bar}$ . Similar to  $T_c$ , the  $T_m$  of  $\text{CO}_2$ -treated iPP decreases linearly with a  $dT_m/dP$  value of  $-0.12 \text{ K/bar}$ . Experimental  $\Delta T_m$  ( $= T_m - T'_m$ ) values, where  $T'_m$  is the melting temperature at a  $\text{CO}_2$  pressure of  $1 \text{ bar}$ , coincide quantitatively with those predicted on the basis of the Flory–Huggins theory.

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